MODEL ENGINEERS' WORKSHOP PROJECTS

Harold Hall

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39. MODEL ENGINEERS’ WORKSHOP PROJECTS

This collection of 18 unique projects for home workshop equipment enables the model engineer to create useful and even essential items that cannot be purchased commercially, including an auxiliary workbench, tap holders, distance and height gauges, a lathe back stop, a tailstock die-holder, faceplate clamps, collets, DTI accessories, sash clamps, low profile clamps and a tapping stand.

Each project is designed to make the model engineer’s task in hand easier than it would have been had the items not been made.

Author Harold Hall is a former editor of the enthusiasts’ magazine Model Engineers’ Workshop, within whose pages all of these projects were originally featured.
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Introduction

Owners of home workshops can no doubt be divided into two groups when it comes to making workshop equipment. For some, typically a model engineer involved in constructing a locomotive, making an item of workshop equipment will be a temporary diversion from the main project in hand. Others, like myself, making workshop tooling is almost the sole activity undertaken. In this case many of the projects will be quite substantial, a rotary table, a dividing head, even larger a gear hobbing machine or tool and cutter grinder. These in many cases will get limited use, but will be put on the shelf and looked at with pride saying, "I made that!"

The items in this book most certainly do not fall into the "I made that!" category. They are though, likely to be hidden in a box somewhere, but brought out frequently to make the task in hand easier than it would have been had they not been made. An important factor in this respect is that most are items that cannot be purchased commercially so making them is the only option should you wish to benefit from having such a device in the workshop. Having made those comments there is though no reason why a reader should not gain satisfaction from completing any of the items throughout the book.

Whilst predominantly tooling, some fall into a more general group, an auxiliary work bench for example and all can be made in a few hours, some much less, and will repay the time taken many times over.

The contents of this book are all items that I have provided for publication in the Model Engineers' Workshop magazine but unlike most of my published work this book does not go deeply into the methods of manufacture, being more of an ideas book. However, should you like a little more guidance on making the tools featured in this book and have access to past copies of MEW then you could look up the issues in which the items appeared. This book is though a complete rewrite with new photographs and drawings (also having modifications). The original work should therefore only be used as a guide to the manufacturing techniques.

Harold Hall 2007
Chapter 1

Auxiliary Bench

This is the simplest of all the items included and without doubt the one that has repaid my time making it by more times over than any other. It is an auxiliary workbench and took me around 15 minutes to make. I did though have a suitable size piece of ply available for the top, but even if you have to cut the top to size 1 hour should be more than enough.

The bench was initially conceived for holding pieces of sheet steel for cutting using a jigsaw, nibbler, etc. This was something I found difficult using my normal bench with it having only one edge available, resulting in clamps and saw wanting to share the same position. The bench, Photo 1, is about 450mm square and has a 75mm x 50mm piece of timber screwed onto the under side which is gripped in the bench vice. Photo 2, shows it being used for its original purpose.

I soon realised that in its elevated position it was also of considerable benefit when marking out, similarly, carrying out delicate assembly work, electronic or mechanical. If you have a small workshop with only limited bench space it will be a worthwhile addition if only to increase your working space, maybe larger may not be a bad idea.

If a long bolt is added to the timber bar this can be gripped in the bench vice and the top tilted to make a small drawing board; Photo 3.

File storage

Whilst in a woodworking theme, the method of storing files on the rear of a cupboard door, Photo 4, is worth considering. It keeps them in the same place all the time so they are easily found and by keeping them apart protects their working faces. Sketch 1 shows the construction in detail. If mounted on a wall rather than on the rear of a door then the lower half could possibly be omitted.

Chuck boards

These were the result of a request from a workshop owner who was beginning to find it difficult to move his lathe chucks to and from the lathe. Additionally, aligning them with the lathe’s mandrel.

Photo 5 shows two boards, one for the three jaw and one for the four jaw. These are used on a gap bed lathe and the piece of wood in front is for placing in the gap to prevent the board tipping with the weight of the chuck. Note how the carrying handles pass in front and behind the chuck ensuring they are secure when being carried.
Photo 3 Used tilted it makes a small drawing board for use in the workshop.

Photo 4 A method of supporting files on the rear of a cupboard door.

Photo 5 These chuck boards make carrying the chucks to and from the lathe an easier operation. Also, whilst on the lathes bed they protect the bed from accidents and holding the chuck at centre height assistin fitting them to the lathe’s mandrel.

To make the board place it against the chuck whilst fitted to the lathe and mark its edge with the shape of the chuck. Start chiselling out the shape, frequently checking it for a close fit under the chuck. The ease of screwing the three jaw chuck onto the lathe’s mandrel is further enhanced by placing a long length of rod in the chuck and loosely closing the drill chucks jaws onto the other end. This will align the chuck with the mandrel making the process a simple one.

Having started with a woodworking theme, in the next chapter we get down to the real purpose of the book, metalworking!
Chapter 2

Tapping Guides

Hand tapping into metal components would at first appear to be a problem free task. This providing the correct tapping size hole has been prepared as an unnecessarily small hole is often the reason for a broken tap!

Attempting the task though it will soon be found not to be as easy as first thought. The main problem is getting the tap to enter in line with the hole’s axis. To achieve this it requires the tap to be viewed in two planes, often not that easy. At best the tapped hole may present a problem when the parts are assembled as a tilted screw attempts to pass through a perpendicular clearance hole. With a number of fixings, assembly may only be possible if the clearance holes are increased in size beyond what would be considered acceptable.

This though is not the only problem, especially with small diameter taps. In this case, as the tap enters further into the hole prepared, it will begin to cut more on one side than the other. As a result, smaller
Size taps are more likely to be broken, even if having the correct threading hole.

Photo 1 shows two forms of tapping guide that, whilst simple, almost eliminates the problems of tapping square. The tap is passed through the appropriate guide and its end located in the hole in the workpiece. With this done, the guide is held onto the workpiece using one hand whilst the other rotates the tap ensuring that the tapped hole is perpendicular to the surface of the component, Photo 2.

The process works well providing the tap can be rotated by a single hand, typically a maximum of 2BA, 3/16in or M5. For larger sizes though, the guide will need clamping in place, Photo 3. In this, the guide is clamped to the workpiece using a toolmakers clamp which in turn is held in the bench vice.

There will of course be some cases where the nature of the workpiece prevents these guides from being used but for most readers, I would assume they would be suitable for the vast majority of hand tapping carried out. Hardly anywhere else will so little time spent making workshop equipment be repaid so many times over in terms of the quality of the final item. I thoroughly recommend these tapping guides to you!
Chapter 3

Guided Die Holder

Rather like the problem starting a tap in line with its tapping hole, as mentioned in Chapter 2, similarly, starting a die at an angle will cause the thread to go out of line with the bar on which it is being made, Photo 1. This is particularly a problem with long threads. Like the provision of a guide to start a tap, a guide to start a die will overcome the problem.

Two methods are possible, one to make a complete die stock having the provisions for guiding it onto the bar being threaded, Sketch 1, and the other to make guide bushes to use with a standard die stock, Sketch 2.

Photo 2 shows a complete die stock for 1 in diameter dies, together with guide bushes. Reference to the drawings for this will show that the bushes are just loosely fitted in the die stock with the forward movement of the assembly keeping the bush in place.

Photo 2. A guided die holder with two guide bushes.

Note though that the workpiece enters the guide first and the die is fitted the opposite way round to normal. However, there is often a sizeable bur on the end of the thread that will prevent the guide bush passing back down the thread, this being more of a problem with larger diameter and coarser threads. However, the bush being loose it can be left at the end of the thread whilst the die is run back towards the start of the thread.

Unfortunately, the method suggested in Sketch 2, has a captive bush and may make removal of the die stock a little difficult on occasions. Also it does not provide access for cleaning the workpiece ahead of the die whilst the thread is being made. Even so, being much easier to make, it may be appropriate for an urgent task or for very infrequent use. I would though suggest that you make guided die stocks for both 13/16in and 1in diameter dies as the system is so much easier to use and produces near perfect results.

Photo 1. A thread that starts out of line will get progressively off axis along the length of the thread.

Sketch 1 GUIDED DIE STOCK
Chapter 4

Large Tap Wrench

Workshop owners will invariably find themselves at some time working, in size terms, beyond what is the norm for the workshop. Typical of this is the need to tap a hole with a thread much larger than the workshop is geared up for. Having to purchase a tap, maybe two (plug and taper) will be expensive enough for a one off application but the need for a larger tap wrench will only add to project’s cost.

Fortunately, making a perfectly adequate wrench is a matter of a few minutes work as the drawing shows. If then it really is a one off job then the screws and materials used can be returned to the raw material stock.

On the other hand, if time is on your side and you wish to make a more professional looking item. Photo 1 shows how this can be achieved whilst still using the same basic design.
Chapter 5

Distance Gauges

The conventional way for establishing a distance using gauges is to use Slip Gauges. These though cover a much wider range than will normally be required in the home workshop, up to a few hundred millimetres depending on how many are stacked together. Of even greater importance, is that they will be much more accurate than will be necessary, typically within 0.00025mm (0.00001in). This all results in an expensive piece of kit.

Like the slip gauges, the distance gauges in this chapter, Photo 1, are intended to be stacked and with this done a range of up to 50 mm is possible, again depending on the number of gauges in the stack. Of course you could make longer gauges than I suggest to increase the range. You will not of course be able to produce gauges to the accuracy of the commercial items and my suggestion is to aim to be within + 0.0 - 0.0025mm (0.0001in) Even this level of accuracy will need particular care to achieve.

Working to such tolerances on a lathe is not easy with two aspects being problematical. First, it will need very fine cuts to be taken to finally bring the part to dimension. This not being easy with the leadscrew being calibrated in 0.025 mm (0.001in) increments when cuts of 0.001 mm (0.00004in) are likely to be required.

When turning outside diameters to precise dimensions it is common practice to set the top slide to an angle of 6°. With this done, traversing the top slide by 0.025 mm will increase the depth of cut by only 0.0025 mm, a ratio of 10:1. For even greater sensitivity, an angle of 0.6° will give a nominal ratio of 100:1. However, whilst the top slide’s calibration for angles will suffice for 6°, 0.6° will need to be set up differently, more about that later.

Having now got a method of setting a fine depth of cut a suitable tool will be required. It should be obvious that you cannot take a cut 0.001mm deep if the tool is slightly blunt and has a radius of 0.002mm on its cutting edge, it will only rub. Only a freshly honed high speed steel tool can provide such a fine edge. The material used for tipped tools cannot, which in any case are often deliberately supplied slightly radiused to provide strength at the cutting edge.

The gauges in this chapter though require accuracy in terms of length rather than diameter and for this the top slide needs to be set with an angle of just 0.6° between it and the cross slide. To do this, with a DTI mounted on the top slide and reading off the faceplate, adjust the angle so that a variation of 0.5 mm occurs on the indicator reading whilst the top slide is traversed 50mm.

You may have to make temporary arrangements for your top slide to be set at this angle. For my Myford series seven the operating handle fouled the cross slide and had to be replaced with a small round knob. Incidentally, using a between-centres test bar rather than the faceplate, a similar method can be used to set the top slide at 0.6° to the lathe’s axis.

Manufacture

With a length of material in the three jaw drill though 6 mm and part off a little longer than the length of the gauge being made. Repeat making at least two of each size. Make a parallel mandrel as per SK1 and use this to hold each gauge in turn for finishing to length. With the first gauge fitted and using a left-hand knife tool face the surface next to the chuck. Do not remove but now with a right hand knife tool fitted, machine the other side precisely to the dimension required Photo 2. To do this, use the cross slide, but the angled top slide to place on the required depth of cut. You will increase the depth of cut on one side by feeding the top slide in and feeding it out will increase the cut for the other side. The different length tubes
Range
The gauges as drawn will provide increments of 0.5 mm up to 50 mm. However, if you would like smaller increments, you could make gauges of 1.1 mm, 1.2 mm, etc. up to 1.9 mm, gauges of 0.1 mm, 0.2 mm, etc. being impractical to make.

Purpose
Having made your distance gauges many uses for them will invariably surface. For me they definitely fit into the category of "why did I not make them earlier?" Only one other item in my workshop beat them into first place in that respect and that is the saddle stop for my lathe. The most used task for the gauges for me is setting the stops on my milling machine, Photo 4, similarly the saddle stop on the lathe.

Outside dimensions
A very simple and very worthwhile addition to the gauges would be to add the outside fingers as shown in Photo 5 for testing outside dimensions. The fingers are seen front of Photo 1.

Hole gauges
Whilst in precision mode, you may like to make some hole gauges as seen in Photo 6, this time setting the top slide at 0.6° to the axis of the lathe. Otherwise there is little difference between making the hole gauges compared to the distance gauges. The drawing shows that gauges have a small reduced diameter at the start to indicate that the hole is approaching the required diameter. I would though add that in my estimation you will find the distance gauges much more used than the hole gauges, a ratio of at least 20:1 in my workshop.

Photo 5 A pack of distance gauges fitted with out side fingers for checking outside dimensions.

Photo 6 Set of hole gauges, it is though unlikely that you will find these as useful as the distance gauges!
Chapter 6

Lathe Tool Height Gauge

If you use a lathe tool holder that requires packing to bring the tool to centre height then you will be aware of the trial and error approach necessary. Even if you use a quick change tool holder its tools will still need setting to centre height, albeit an easier operation. A simple fixed height gauge will ease the problem if the tool is low as the error can be checked using feeler gauges, if high though this will not be possible.

The gauge, Photo 1, enables the error to be determined, high or low, and from this suitable changes to the packing height can be determined. For my part, tool holders requiring packing do not deserve the bad press they get from many workshop owners. The answer to the problem is to be organised and have a generous supply of packing already available, cut to the appropriate size and scribed with their thickness. With a good supply of packing thicknesses, setting the tool to the required height should be relatively easy. Remember that packing need not be metal, as hard plastic will do equally well. Because of this, much modern packing, food containers, CD cases, etc. will yield a wide range of shim thicknesses.

The basic principle of the gauge is that the testing surface can be raised or lowered by precise amounts as indicated by the micrometer type barrel. From this reading, the change in packing thickness
required, an increase or decrease, can be determined and the necessary changes made eliminating the need to make trial cuts. On final assembly the gauge is set to read zero at centre height so that the degree of error can be determined, either plus or minus.

The gauge is provided with two testing surfaces enabling top slide, Photo 2, and rear toolpost tools, Photo 3 to be tested. Photo 4 shows the parts ready for final assembly. There should be no problem with this providing that you have ensured that the important diameters, including the threads, are concentric.

The thread's pitch will need to be chosen to suit your workshop's preferred units, Imperial or Metric. For Imperial, a 1/4in x 40 TPI model engineer's thread will be ideal as this will give 25 one thou (0.001in) divisions, being the same as on an Imperial micrometer. If metric, then an M6 thread having a pitch of 1mm will be the best choice.

The assembly drawing shows that between the lock nut (2) and the arm (3) there is a spring washer with a plain washer on either side. This enables small adjustments to the height using the barrel without having to adjust the nut. Taking a standard spring washer and bending this to increase the set will increase the adjustment available before having to move the nut. The washers enable the arm to be rotated freely.

To calibrate the gauge, place a piece of steel in the chuck and turn a short length accurately to 4.00mm, or 0.100in, depending on the units chosen. Lower the gauge until the arm just contacts the test piece and mark the barrel zero where its calibration coincides with the vertical calibration line on the post. Now lower the barrel by two turns exactly and scribe a line round the post at the end of the barrel. This then is the setting for centre height. The amount by which the zero calibration deviates from the vertical line on the post indicates the amount that the arm is above or below centre height.

Whilst it is always recommended that the tool should be on centre height it is important that it is not above else the front edge will rub, especially for very light cuts and on smaller diameters. For my part, because of this, I always err on the side of it being below centre, or above for a rear toolpost tool. Having made the gauge this degree of accuracy will be quite easy to achieve!
LATHE TOOL HEIGHT GAUGE

DIMENSIONS GIVEN ON DETAIL PARTS SHOULD SUIT A LATHE CENTRE HEIGHT OF BETWEEN 70mm AND 100mm.
CHANGE PARTS 1 AND OR 6 FOR OTHER CENTRE HEIGHTS.

HARDWARE
1 PLAIN WASHER 2 OFF
2 SPRING WASHER
BOTH TO SUIT CHOSEN THREAD SIZE

MATERIAL 50 DIAMETER STEEL 230M07
QUANTITY 1 OFF

POST 1

A. M6
B. VERTICAL CALIBRATION LINE
C. THREAD TO SUIT CHOSEN UNITS, SUGGEST 1/4" X 40 TPI FOR IMPERIAL AND M6 (1 mm PITCH) FOR METRIC
THREAD C AND 9.9 DIAMETER MUST BE CONCENTRIC

MATERIAL 12 DIAMETER STEEL 230M07
QUANTITY 1 OFF

BARREL 5

A. CALIBRATE TO SUIT CHOSEN UNITS
B. FIT FEED NUT(4) USING TWO PART RESIN ADHESIVE

MATERIAL 15 DIAMETER STEEL 230M07
QUANTITY 1 OFF

ARM 3

THREAD TO SUIT POST PART 1
THREAD MUST BE CONCENTRIC WITH 9.95 OUTSIDE DIAMETER.

MATERIAL 12 DIAMETER STEEL 230M07
QUANTITY 1 OFF

FEED NUT 4

LOCK NUT 2

MATERIAL 20 DIAMETER STEEL 230M07
QUANTITY 1 OFF
Chapter 7

Lathe Back Stop

Having to turn even a single part to a precise length can be a minor problem with the normal approach as follows. Make the part ensuring that it is a little on the long side, remove from the chuck and measure the length to determine the amount to be removed. Return the part to the chuck, but obviously it will not be possible to put it back exactly in the same position. Because of this, it will be necessary to bring the tool up to the end of the part before moving the top slide forward by the amount to be removed. If however, the part could be returned exactly to the same place the top slide could be just moved forward and the result would be more certain. This is where the benefit of a back stop surfaces as this permits workpieces to be returned to the chuck in exactly the same axial position. However, the real benefit of a back stop is where a batch of identical parts is to be made. In this case the parts will be more accurate and completed in a shorter time.

Photo 1 The parts that make up the back stop.
The Stop piece (B6) is also useful to support a part held in the three-jaw chuck but where only a short length is available for gripping. Typically, a part whose thickness is thin compared to its length.

When in use the inner collet (B1) is pulled into the body (B3) by the Handwheel (B2) closing the inner collet onto the Stop bar (B4) but simultaneously expanding the main body into the bore of the lathe's mandrel, thereby firmly holding them in place. The drawings suit a lathe with a mandrel bore of 5/8in for other bores you will need to change some dimensions.

Manufacture is straightforward and needs no comment. Photo 1 shows the parts, except for the stop bar support (B5), that make up the device.
Chapter 8

Tailstock Die Holders

The subject in this paragraph is certainly one that can be purchased commercially and relatively cheaply. If this is done though, it is likely that a single one will be acquired and the die changed each time a change of thread is required. The holders in this chapter are though very simple to make, especially if made in quantity, and therefore suggest one for each regularly used thread size would be a good idea. This would probably make it financially worthwhile to make them in the shop rather than purchase. In either case you will have to make the tailstock adapter for supporting the holders. Also, the commercial holders will need drilling for Tommy bar operation as they are intended for machine rather than manual operation.

Photo 1 shows a set of holders housing M3, M4, M5, M6, M8 and M10 together with two spares for occasional use with other sizes, Model Engineers 40 TPI typically. The photograph also shows an adapter having a Number 2 Morse taper shank. If you do not want to be involved in turning a taper shank then making one with a short parallel portion for holding in the drill chuck would be another approach, though not ideal.

Manufacture

The essential requirement for these holders is that the bore for the die and the shank should be concentric. The easiest way of achieving this is to make the bore and to turn the shank with a left-hand knife tool, doing this without removing the part from the chuck. This though will leave a small stub of steel in the chuck after parting off that may not find a use. The following method will avoid any wastage of material.

Cut the required number of pieces of steel, just longer than the finished item. Mount in the chuck and face the first end. Also commence to machine the shank but leaving it about 1 mm larger on diameter and shorter on length, remove, turn end on end, reft. Now, face the other end and drill through with the drill size quoted, followed by making the bore to house the die. Repeat for as many holders as you decide to make.

Photo 1 Two sizes of die stock 13/16in and 1in fitted with dies for M3 through to M10. Two holders without dies are for use with dies used only occasionally.
Photo 3 You do not need an expensive dividing head for much of the work in the home workshop. This one is perfectly adequate for the Tommy bar and grub screw holes. The holder is being held on the same stub mandrel as was used for turning the shank.

Place a short piece of steel in the chuck and turn a short stub mandrel a close fit in the bore for holding the die. Make the stub mandrel, say 3 mm long, allowing the flange to mate with the end of the holder. Drill and tap M6. Do not remove until all the holders have been completed. If you work on the larger holders first, the stub can then be reduced for use with the smaller holders.

Fit the first holder and finish turn the shank to the appropriate diameter and length and skim the outer diameter, Photo 2. This process ensures that both the shank and die seat are concentric. Repeat for the remaining holders.

The remaining operations need no comment though you may be interested in my set up for drilling the Tommy bar holes, Photo 3. Note that this uses the same mandrel for holding the parts for drilling whilst still fitted in the chuck.
Chapter 9

Face Plate and Angle Plate Clamps

The main problem with holding workpieces, both on the faceplate and angle plate, is their small size and limited number of fixing slots. Their small size in particular makes the clamps used on the milling machine table invariably too large for these situations. The clamps in this chapter seek to overcome this problem which takes a fresh look at the method to use. The system will be described in terms of its use on the faceplate where there are particular considerations, when used on the angle plate the method will be much the same though less demanding.

Photo 1 A range of parts that make up the clamping system. However, for maximum benefit more of each part should be made than shown.
A single clamping set-up will comprise a clamp bar with a central clamping stud and with one end holding the component whilst the other rests on a packing piece of some form. This needs to be just higher than the component. Whilst this is perfectly acceptable on the milling machine table it has safety considerations when used on the faceplate. In this case, the rotation of the faceplate will be attempting to throw out the packing and if not fully secure for some reason could be potentially very dangerous. Because of this, the clamps in this chapter have been designed to be both compact, and for the packing to be captive.

Sketch 1 illustrates the basic design whilst Photo 1 shows a range of typical parts. As the packing is tapped it shows that the packing and clamp screw are both captive prior to clamping the workpiece. This is a major advantage when fixing the first clamp as with both the packing and the clamp screw being firmly fixed there is still one hand to hold the workpiece and one to tighten the clamp screw nut. After having fixed the component in place with two or more clamps, individual clamps and packing pieces can easily be loosened to move them into better positions.

As the packing has to be just higher than the workpiece a large number of different height packing pieces would be required. To minimise this, height increasing bushes are made in a range of heights so that they can be used in combinations and with the packing pieces, also made in a few heights, to cover a range dimensions with the minimum number of parts, SK 2 illustrates this. The height increasing bushes have clearance holes.

As the number of fixing slots is limited making it difficult to get the clamping screw in precisely the best place in some cases, additional flexibility is achieved by a second hole in the packing pieces and height increasing bushes. This set up is seen in SK 3. This though results in the clamping screw being nearer the packing than the workpiece, which is not ideal. The set up should therefor only be used where that in SK 1 is not possible, preferably then only as a back up where some clamps as per SK 1 are also being used. Photo 2 shows a typical application where the parts are being used on the faceplate.

With a suitable screw added, the packing pieces would also make useful mini jacks, Photo 3. These could have uses in a wide range of situations. The clamp plates could also be used alone in conventional clamping set-ups on the milling machine.

All the parts are simple to make and would benefit from generous quantities being made. In this respect, it is easier to make an extra one or two of an item at the initial stage than going back and making more later. Some thoughts in terms of production methods would help to speed up their manufacture.

To gain maximum benefit from using these clamps on the faceplate, why not make the Faceplate Balancing Fixture described in Chapter 13.
Chapter 10

Lathe Collets

Commercially available collets are now so relatively cheap that making collets, other than as an interesting project, may seem pointless. However, holders for the collets in the ER series mostly come with Morse, or other, taper shank and do not allow bar material to pass through them. They are therefore only suitable for short workpieces although there are now signs of this shortcoming being addressed by the tool suppliers. Even so, I am sure there will be some who will say that there is no need to make collets in view of them being readily available, a comment with which I have some sympathy. I have though included this chapter, as some of the items are common with the thin piece collets in Chapter 11, items that to my knowledge are not readily available commercially.

The conventional collets with holder

Photo 1 Conventional collets and collet body.
can be seen in Photo 1 and reference to Chapter 11. Photo 2, shows that both systems use the same body that mounts to the lathe spindle nose.

As I explained in the Introduction it is not my intention to go deeply into manufacturing techniques for items in this book and this item is one where the reader should have no problem if conversant with basic turning methods. Concentricity is the most vital consideration and the following sequence would be worth following.

Make sufficient collet blanks producing at this stage just the 16mm bore, the rear parallel portions and the 20° taper. Drill through 3.5 mm and part off. If you carry out this stage using a fixed steady you will not end up with a small stub after making each one. Leave the top slide set at 20°.

Now fit a short length of say 25 mm diameter steel in the three jaw and bore 19.00 mm diameter 3 mm deep, drill and tap the centre M3, do not remove from the chuck. This can then be used to hold each collet in turn to produce the 16mm diameter and the 10° front face. Do not set the top slide at 10° but set the knife tool round at this angle as illustrated in the drawing showing this set up. Make the angled face in stages taking only a very light finishing cut over the complete width.

Make the collet closing ring but again do not move the top slide from its 20° position but finally set the boring tool round to produce the 10° angle using its front face. As with the collet this face will have to be machined with caution, especially in this case due to the overhang of the boring tool. Whilst it is essential that the 20° angle is the same for both the collet and the collet body the 10° is not so important, hence the method proposed.

The final major process is to make the lathe collet body making the 19.00mm
bore and the 20° face last. This will ensure that they are running perfectly true for boring the collets. You will of course have to use an inverted boring bar, machining on the rear face for producing the angle. Fit the closing ring and finish its outer surfaces.

Now fit each collet in turn and bore, not drill, to the sizes required. Slit the collets, drill holes for Tommy bars, etc. and the job is done. The jig made for holding the collets while turning the front face can also be used for holding them whilst they are being slit.

**Collets for square materials**

Providing you have a collet system for your lathe, be it that above or some other, the collets in this chapter will give you the answer to a very difficult problem. That is, how to hold small square bar, particularly very small, say 3mm.

Making a complete collet for round material is quite a lengthy task, but if square, very lengthy, as a broach would have to be made to produce the square. There would then still be the problem of ensuring that it was concentric.

The idea proposed for using four individual jaws in an existing round collet overcomes the problem with ease and the manufacturing time will be no more than half an hour.

Take four lengths of square material of suitable size and length and hold them in the four jaw separating them with thin card as SK1 shows. Turn a length, say 30mm for smaller sizes, to fit the chosen round collet. Then turn a further 3mm to a larger diameter to eventually produce a head and part off at this length. When making the jaws to this stage it would be a good idea to make a few additional sets of jaws for eventual use as other square sizes need to be held.

Now all that is needed is to produce a flat on the corners that will eventually grip the square material. For larger sizes doing this on the milling machine is probably best but for smaller sizes filing it whilst held in the vice will not be difficult. Having worked out the dimension, just place a micrometer across the curved surface onto the flat and at points along the length of the jaw to check progress, SK2 details how the required dimension can be arrived at. Do not assume that you just remove half the width of the square, as this does not take into account the width of the space between the individual jaws when in use.

**Photo 2** shows a set of jaws in a collet chuck holding a small square section and separately two sets of jaws made for other sizes. Whilst as a last resort the four jaw chuck could be used the collet system will win hands down when making very small parts in large numbers, square nuts for a model horse drawn cart for example. Also, running the collet at a very high speed for the task will be much more pleasant than running a large four jaw at such speeds.
Chapter 11

Thin Piece Collets

For most, there will come a time when a thin piece collet will be an essential item for a particular task in hand as often there is no acceptable alternative. The workshop owner may of course attempt to get by with a temporary solution such as those shown in Photo 1 and which are used in the three of four jaw chuck. They will though fall short of the ideal in terms of accuracy and security of the hold provided.

The collets described in this chapter Photo 1 Two thin piece collets for use in the three jaw chuck. These are not idea but are an option for a one off application. seek to provide a better solution and are shown in Photo 2, which includes the parts, excluding the draw bar, that make up the system. These collets will hold material up to 28 mm diameter. From this, and Photo 1 in Chapter 10 it can be seen that both collet systems use the same body. However, if you are just making this part of the system, only the body will require making plus the handwheel and draw bar. Even for this it will not be necessary to produce the external threads, etc. on the body.

Photo 2 The parts that make up the system at the smaller diameters. There is also a draw bar that is not shown in the photograph.

As Photo 2 shows, make a few collets still left long for repeated boring to sizes required as later projects dictate. You can though make at this stage one to take your most common sizes as seen, centre of the photograph.

The collets with removable jaws, Photo 3, are more complex but will allow larger diameters to be machined. Again make some spare jaws (left of the photograph) for possible boring at other diameters at a later date. Of course, being soft, even the already bored collets can be re-machined for other diameters. With this and the other thin piece collets, it will be necessary to make a close fitting plug (centre of Photo 2) to go into the bore to stop the slots closing when subsequently boring out to additional or new diameters. This is best made at the same time as the collets are made.

The thin piece collet system is particularly useful as photograph 3 in Chapter 5 illustrates. In this a distance gauge, 2.0 mm thick, is having a hole drilled

Photo 3 A collet for larger diameters, also a spare jaw for possible future use.
Photo 4 This photograph shows that these collets can be used at longer lengths. Their use really being where only a small length of the workpiece is available for gripping in the chuck.

to a larger size but was similarly used down to 0.5 mm thick, something that would be quite difficult by any other means.

Photo 4 shows the removable jaw collet in use and illustrates that the term 'thin piece collet' is not exactly accurate. They are mainly for use in a situation where only a small portion of the workpiece is available to be gripped in the chuck or collet. Of course, the further the item projects from the collet the more cautious one must be in terms of depth of cut and feed rate. I have though taken a cut of 3mm wide at 40mm diameter and 25mm from the collet, with a sharp tool, and a delicate feed, I must admit.

The part being held though must have a square corner, in which case a depth of bore of 1 mm in the collet should suffice. For less precise workpieces and or the need to work some distance from the collet, say more than the part’s diameter, then a bore depth of 2mm would be a wise precaution.

STEPPED COLLET

GENERAL PURPOSE COLLET

PLUG

MAKE STEPS AS REQUIRED. 2MM ON DIAMETER X 1MM DEEP SUGGESTED

MATERIAL 30 DIAMETER STEEL 230M07

STEP TO BE BORED WHEN REQUIRED TO SUIT TASK IN HAND

MATERIAL 30 DIAMETER STEEL 230M07

TO BE A CLOSE FIT IN THE GENERAL PURPOSE COLLET BORE

USED TO PREVENT COLLET CLOSING WHEN SUBSEQUENTLY BORED TO SUIT TASK IN HAND

MATERIAL 20 DIAMETER STEEL 230M07
**Handwheel**

Material: 50 diameter steel 230M07

Use two part resin adhesive to fix handwheel to handwheel bush

Quantity 1 off

**Handwheel Bush**

Holes: A. 7 x 45 deep  B. M6

Material: 25 diameter steel 230M07

Notes:

X. To be a free fit in the lathe's mandrel bore

Quantity 1 off

**Drawbar**

Length to suit lathe's mandrel

Material: 25 diameter steel 230M07

Quantity 1 off

**Removable Jaw Collet**

Holes: A. 6 holes 83 x 6 deep on a 24 piece

All dimensions not given are as per the stepped collet

Material: 35 diameter steel 230M07

**Interchangeable Jaws**

Make dimensions to suit parts to be held

If the part to be held has square edges a bore 1 mm deep should be adequate otherwise make bore 2 mm deep

For small diameters bore may break into counterbores

Material: Steel 230M07

Diameter to suit
Dial Test Indicator Accessories

The term "Dial test indicator Accessories" greatly understates the possibilities with the subject of this chapter. As will be seen it can satisfy a wide range of requirements and is as a result the largest project in the book. However, it is by no means the most complex. Central to the equipment is the flexible joint and whilst this is available commercially most of the other items will have to be shop made.

Flexible joints

Photo 1 shows the full range of parts though the reader will only have to make those items that are likely to be useful in the workshop where they are to be used. However, do make at least 6 flexible joints (AS1) as you may be surprised just how many you will use, especially if you keep some of the assemblies ready made up for use, that in Photo 2 being typical. In this a DTI is prepared for use on the lathe being coupled up to a holder in my quick-change system. The indicator itself can of course be rapidly removed for use elsewhere but still leaving the bulk of the set up intact.

Some DTI's have mounting barrels that are smaller than the 8mm diameter of the bars so you may need some joints with one half having a smaller hole. It may even be a good idea to make a few without a hole so that it will be easy at a later date to make an arm clamp (F1) with a different hole size to those available. As the joints can easily be dismantled it will be possible to mix and match diameters as required. Note that the taper bit, SK1, is for making the tapered counterbore in each half of the flexible joint.

Also, you will need a range of arm (A1) lengths and would suggest at least three of each size.

Mounts

Having made your joints and arms they will be of little use without the means of mounting them and it is here where the absence of easily available commercial
items makes it necessary to manufacture the provisions in the workshop. **Photo 3** shows how a dial test indicator can be firmly mounted on the lathes cross slide using its T slots. T slots are likely to be larger on other machines so that more than one size of T bolt will be required. These are parts M1, M2, M3 and M4, you may however need to change the sizes of M2 and M3 to suit your machines. The large washer is to support the General Purpose Mount (M1) when used with a large T slot.

Mostly, when used on a milling machine, the dial requires to remain stationary whilst the table moves. This requires the assembly to be mounted off a non-moving part of the machine, **Photo 4** showing a possible solution. In this, the mount (M5), is mounted off the down feed stop bracket where it can be left permanently.

As an alternative to using the T slot mounting method on the lathe, the right angle mount (M7) could be used directly off the top slide or even permanently mounted into a quick change tool holder for rapid use as was seen in **Photo 2**. Another rapid method of mounting and removing an assembly is to use the G clamp mount, **Photo 5**. This comprises G1, G2, G3 and G4. The Vee Pad (G5) is used when mounting it onto a round support as in the photograph.

Sometimes it is useful to be able to use the system free standing, **Photo 6**. For this it will be necessary to make the base (B1). This simple component opens up many more possibilities. **Photo 7** shows it as a holder for a magnifying glass for intricate work. **Photo 8** shows it being used as an instrument makers vice, very useful for those who do modelling or other tasks in the smallest scales. If you are into electronics then using it for
assembling Photo 9 and soldering Photo 10 would be very well worthwhile.

Photo's 8, 9, 10 and 11 are seen using the clamp C1/C2. These use two screws for securing the item being held, in the same way as a standard toolmakers clamp. Photo 11 shows one being used for holding a machine guard.

Another very useful addition is the adjustable arm (AS2) as seen in Photo 3. This is a little more complex than other items but the only crucial item is that items A5 and A7 are adjusted so that there is no back lash present. When set, it is locked using setscrew part H1.

Above left: Photo 7 A magnifying lens stand.

Right and Below: Photos 9 and 10 Being used for electronic assembly.

There are a few other items, locking screws, etc. that have not had a mention. However, the photographs together with the drawings should make their use obvious. No doubt, the reader will find other useful applications, perhaps even designing other parts to augment the system

Left: Photo 8 Being used as an instrument makers vice for delicate work.

Whilst some items in the system find only occasional use the basic kit for mounting a dial test indicator typically gets very frequent use and must rate in my top three workshop items that I have made. The others being the distance gauges (Chapter 5) and my saddle stop for my lathe.
Photo 11 Holding a light weight machine guard.

```
NOTES
USE G5 AS REQUIRED
SECURE G2 INTO G1 USING ADHESIVE
CLOSE G4 ONTO G3 AFTER ASSEMBLY

G CLAMP MOUNT
```

A. MAKE IN VARIOUS LENGTHS, SUGGESTED, 50, 100, 150 AND 200
MATERIAL 8 DIAMETER STEEL 233M07
QUANTITY MINIMUM 4 OFF 50 AND 100 LENGTHS
AND 2 OFF 150 AND 200 LENGTHS.

ARMS A1

```
MATERIAL M4 X 30 HEX HEAD SCREW
QUANTITY SUFFICIENT FOR THE NUMBER OF CLAMPS MADE
```

ARM CLAMP F1

```
SHAPE GENERALLY AS SHOWN
USE ADHESIVE TO FIX ARM
MATERIAL
10 DIAMETER STEEL 233M07
6 DIAMETER STEEL 233M07
QUANTITY AS REQUIRED
```

FLEXIBLE JOINT ASSEMBLY AS1

```
MATERIAL 8 DIAMETER SILVER STEEL
HARDEN CUTTING EDGES
TAPER BIT SK1
```

CLAMPING NUT F2
PART VIEW SHOWING POSITION OF A4

H1 M3 X 6 SOCKET SET SCREW 1 OFF
H2 M6 NUT THINNED TO 3MM 2 OFF

ADJUSTABLE ARM A2

MATERIAL 12 DIA. STEEL 230M07
QUANTITY 1 OFF

NUT A7

BODY A6

MATERIAL 10 DIAMETER STEEL 230M07
QUANTITY 1 OFF

SCREW A5

ARM CARRIER A2

MATERIAL 8 DIA. STEEL 230M07
QUANTITY 1 OFF

ARM A1

FEED NUT A4
Faceplate Balancing Fixture

Having fixed your workpiece in the correct position on the lathe’s faceplate it is still essential to balance the assembly by the addition of suitably placed weights. This is necessary else it will often be impossible to run the lathe at the speed required. Accurate balancing will certainly be necessary where the operation requires the lathe to run at a high speed.

Whilst balancing can be carried out on the lathe, the drag on the bearings and the problem of keeping the belts clear of Photo 1 The finished faceplate balancing fixture.

Right: Photo 2 In the vertical position as used for balancing.

Right: Photo 3 Placed in the horizontal position, loading the faceplate is much more easy than whilst mounted on the lathe.
bracket and then used to position the workpiece precisely as Photo 3 illustrates.

The design achieves its free running ability by incorporating shop made bearings using 4mm balls. These can be obtained cheaply from your local cycle repair shop.

Most parts required are easy to make and need no comment but for others concentricity is vital. The following give a very brief idea how this can be achieved but does not though detail the complete manufacturing process. Do also study carefully the spindle assembly drawing so that you are fully aware of the requirements in terms of accuracy, concentricity, etc. Also, the spindle nose is dimensioned to suit a Myford Series Seven lathe, for other lathes you will no doubt have to change some dimensions.

Spindle (3)
The important requirements for this are that, the face plate mounting, the angled surface of the bearing and the 14mm diameter on which the end bearing is mounted are all concentric. Ideally, to achieve this, the part should be machined between centres. The prototype also has a Morse taper socket though I have never found this to be of use. Because of this I have not included it on the drawings, if however you wish to include this it places additional complications in terms of machining the spindle.

End bearing (8)
Concentricity of the angled bearing surface and the 14mm bore are the essential features and machining them at the same visit to the lathe will ensure this. The bore must also be a very close fit on the spindle.

Outer Bearing (4)
This is probably the most complex as the two bores that need to be concentric are at opposite ends of the component. Bore one end but do not produce the through bore of 30mm diameter. Remove from the chuck, turn and refit, and bore the other end 28mm diameter 25mm deep, drill through 8.5mm diameter, remove from the chuck.

Mount a short piece of 50mm steel in the chuck and make a stub mandrel a very close fit in the 40mm bore already made and long enough so that the end of the mandrel, suitably faced, contacts the base of the bore. Do not remove the mandrel from the chuck but drill and tap M8. The outer bearing can now be fitted to this and the 40mm bore on the second end made. This process will ensure the two bores are concentric and their bases parallel. Remove from the mandrel and refit into the chuck and through bore as per drawing.

Photo 4 shows all the parts prior to final assembly. Incidentally, the Angle (10) can easily be removed and with this done it may find other uses, on the milling machine maybe.

Of all the items in this book, this one improves the task being undertaken by more than any other, only the faceplate clamps, Chapter 9 coming close.
HOLE SIZES.
A. 5.1 DRILL AFTER ASSEMBLY.
REQUIRED IN ONE END PLATE ONLY.
SEE ASSEMBLY DRAWING.
B. M5 X 10 DEEP. 2 OFF.
MATERIAL. 60 X 10 STEEL 070M20.
QTY. 2 OFF. SEE NOTE RE HOLE A

END PLATES 1

HOLE SIZES.
A. 5.5
C. BORE 9 dia. X 5 DEEP 4 OFF.
MATERIAL. 60 X 10 STEEL 070M20.
QTY. 1 OFF.

BASE PLATE 2

NOTE, NOSE DIMENSIONS SUIT A MYFORD SERIES SEVEN
FOR OTHER LATHES CHANGES MAY BE NECESSARY

HOLE SIZES. A. 5.1. DRILL AFTER ASSEMBLY WITH END
PLATE AND BEARING.
MATERIAL. 40 DIAMETER STEEL 230M07. QTY. 1 OFF.

SPINDLE 3
Chapter 14

Low Profile Clamps

Whilst other clamping methods will find much more use on the milling machine, the clamps in this chapter will make some tasks possible which would otherwise be almost impossible. Photo 1 shows a piece of black iron that was too large for the available vice having its upper face surfaced.

Even though the clamps are referred to as "low profile" as the clamping action is close to the machine's table; they can be used with much thicker materials providing the necessary precautions are taken.

1. Most important is, that once the height of the component becomes more than a few millimetres higher than the clamp itself then the component's foot print on the machine table must be appreciably longer than its height. Typically, if machining at 40mm above the worktable then a workpiece length of 100mm should be considered a minimum.

2. Never use less than two clamps, preferably more when machining well above the worktable.

3. Always limit the cutting depth/feed when working well above the machine table.

Photo 1 Type four clamps being used to hold a piece of black iron for surfacing.
Photo 2 The five types of clamps, type’s one to five left to right.

Having made those comments it is worth bearing in mind that a higher fixed jaw will help considerably.

With these precautions being observed then the clamps will be found to be a very valuable addition to one’s workshop equipment.

The clamps
The common feature of all five clamps, Photo 2, described is the method in which they are held in position. Reference to the assembly drawings will show that each have a grub screw (H1). This is used to firmly locate the clamp in place by tightening the screw down into the base of the tee slot. In other respects each clamp uses a different approach to providing the clamping action. The five assembly drawings should make this clear.

Clamp three has the advantage of being far the easiest to make and works well but with one limitation, that is, it can only clamp surfaces that are at nominally right angles to the tee slot. Clamps 4 and 5 have the same limitation but have the advantage that the clamping action tends to hold the workpiece against the worktable as well as the fixed jaw. Clamp 4 is particularly good in this respect.

Clamps 1 and 2 do though have the advantage of being able to hold non-rectangular workpieces due to them both having rotating jaws. If though the workpiece has one straight edge it maybe that the fixed jaws can accommodate the irregular shape in which case clamps 3, 4 and 5 may be in with a chance.

If all things considered you decide not to make any of the clamps detailed then clamps rather similar to clamp 1 are to be had commercially.

I doubt if many readers will wish to make all five types but would suggest that you make a minimum of four clamps. If you wish to experiment then you could make more than one type. In this case I would though recommend a minimum of...
two of each type made.

The dimensions suit a 16mm wide tee slot you will need to change at least some dimensions for other slot sizes.

One point that is not covered on the drawings is that for clamp 1 the screw (H2) is to be fitted into the cam (12) using a two-part resin adhesive. If you would like to be a little more confident regarding this you could drill across the joint between the outer diameter of the screw head and the inner diameter of the cam and fit a close fitting pin, again held with adhesive.

**In use**

Using the clamps is straightforward but you only need to use the clamps on one side of the part being held. On the other side a fixed jaw, or jaws, should be provided which must be firmly clamped with a through screw. Do not use an overhead clamp to hold the jaw as the clamping pressure can be quite large in which case the fixed jaw may move.
CLAMP ASSEMBLY 4

HARDWARE
1. M8 X 16 SKT GRUB SCREW 1 OFF
2. M5 X 16 SKT CAP SCREW 1 OFF

CLAMP 41

HOLE 5.5 DIA. C/B 9 DIA.
MATERIAL
16 X 8 STEEL 070M20
QUANTITY
1 OFF PER CLAMP

CLAMP ASSEMBLY 5

HARDWARE
1. M8 X 16 SKT GRUB SCREW 1 OFF
2. M6 X 16 SKT CSK SCREW 1 OFF

CLAMP PIECE 52

HOLES SIZE 8
CSK 14 X 90°
MATERIAL
16 X 6 STEEL 070M20
QUANTITY
1 OFF PER CLAMP

T NUT 42

HOLE A. M8 1 OFF
B. M5 X 10 DEEP 1 OFF USE CLAMP PIECE AS A JIG TO POSITION
MATERIAL 32 X 25 STEEL 070M20
QUANTITY 1 OFF PER CLAMP

T NUT 52

HOLE SIZES A. M6 X 12 DEEP 1 OFF
B. M8 1 OFF
MATERIAL 25 SQ. STEEL 230M07
QUANTITY 1 OFF PER CLAMP
Chapter 15

Engineers Sash Clamps

Sash clamps, or should be cramps, are in commercial terms a product for the cabinetmaker. However, I decided that a smaller, but more robust, version could be of use in the engineer's workshop and the result is seen in Photo 1.

Since having made these their use has mostly been as a milling machine table vice for large items, a task that they perform well as seen in Photos 2 and 3. However, they are not limited to this task as Photo 4 shows. In this, the two ends of the head assembly for the tapping stand, Chapter 16, are being held together whilst the adhesive sets.

Manufacture is straightforward other than to say that the holes along the length of the bar must be equally spaced. In terms of length you may like to make the clamps longer by a few more pitches as I have found that this would have been useful on a number of occasions.

The two bars as seen at the front of Photo 1 are for securing the clamps onto the milling machine table as seen in Photo 2. I have not drawn and dimensioned these, as they need to be made to suit, in particular the pitch of the holes to match the spacing of the tee slots on your machine.

Above: Photo 2
Being used to hold a large flat plate.

Right: Photo 3
Being used to hold a large casting.
Photo 4 Use is not confined solely to the milling machine. In this case three parts are being held whilst the adhesive is being used. See Head Assembly Chapter 16.

NOTES
- DRILL RIVET HOLES IN PARTS 7 AND 10 AND ONE OFF SIDE PLATES 6 AND 9 ON ASSEMBLY. USE PINS 1 AND BAR 8 TO ALIGN PARTS

THE QUANTITIES ON THE PART DRAWINGS ARE FOR ONE CLAMP ONLY. IT IS SUGGESTED THAT TWO CLAMPS SHOULD BE MADE FOR USE IN PAIRS AS A MACHINE VICE.

HARDWARE H1 M4x6 SOCKET GRUB SCREW  ENGINEERS SASH CLAMP
Chapter 16

Tapping Stand

Whilst the tapping guides described in Chapter 2 will be of considerable benefit for many applications, the tapping stand here has some very worthwhile advantages. The major feature of the stand, Photo 1, is that the tap is automatically fed at the pitch of the thread being cut. In simple terms, this means that the tap only needs turning as the stand will feed the tap into the workpiece.

The main advantage of this is that there is no need to use a taper tap, as a plug tap will start the thread perfectly adequately. This particularly makes it a simple operation to tap shallow blind holes a task that is otherwise difficult due to it not being possible to use a taper tap. Not only does it achieve this aim but also it does it perfectly, no partial threads at the commencement of the hole, as there would likely be if hand tapped using a plug tap only.

Another advantage is its ability to accurately start a thread into a non-flat surface where the simple guides would be of no help. Photo 2 shows a typical example. In this case, one of the tailstock die holders featured in Chapter 8 is seen being tapped.

For one or two holes into a flat surface then using the simple guides will be more than adequate. However, for more holes,

Photo 1 The complete Tapping Stand.
screw will be required. The self-feed can though be overridden if a one off special pitch thread for which you have not made a feed screw assembly surfaces.

To gain most benefit from using the stand, or any other hand tapping for that matter, do carefully choose the tapping drill size used. Unfortunately, most charts do not quote the resulting thread depth and in most cases quote a drill that is unnecessarily small. A thread depth of between 60 and 70% depth will be more than adequate for all but the most demanding applications. It will also reduce appreciably the likelihood of a broken tap.

**Manufacture**

Manufacture is easy, only concentricity being important with the feed screw components (7 and 8) tap holder (11) and the tap carrier (10). With the later, the bores at both ends must be concentric and this will need the bore at one end to be made whilst the part is held on a stub mandrel at the other.

The feed screws do not need to be a close fit in the thread in the tap carrier spindle (8). In fact, a loose fitting thread will give some leeway in terms of concentricity. Because of this the design proposes using off the shelf screws for use as the feed screw.

**Using**

In use, operation is straightforward. However, for larger threads and or smaller components, a vice to hold the workpiece should be used. For larger threads, say M6, then the component should be firmly clamped to the table allowing both hands to be used to turn the tap. The slotted table makes this easy but you may even like to make some tee nuts to make this even easier than using just nuts and washers.

**A final comment**

Having arrived at the book’s end I do hope you have been able to make some of the items illustrated and found them as useful as I have!
TAPPING STAND

HARDWARE
H1 M5 X 8 SOCKET GRUB SCREW 2 OFF
H2 M5 X 25 SOCKET CAP SCREW 4 OFF
H3 M4 X 12 SOCKET CAP SCREW 10 OFF
H4 FEED SCREW
DIAMETER AND LENGTH TO SUIT PITCH
H5 M4 X 6 SOCKET GRUB SCREW 1 OFF
H6 M3 X 4 SOCKET GRUB SCREW
4 OFF PER TAP HOLDER (11)
H7 M4 X 10 SOCKET CAP SCREW 1 OFF

MATERIAL 40 X 20 STEEL 070M20

DRILL HOLES B AFTER ASSEMBLY WITH PARTS 3, 15, 12 AND 13 NOTING DIMENSIONS ON HEAD ASSEMBLY DRAWING.

HOLES A. 16 B. 10 2 OFF C. 5.2

QUANTITY 1 OFF
COLUMN BRACKET 14
LOCKING LEVER 1

MATERIAL
16 DIAMETER
STEEL 230M07

5 DIAMETER
STEEL 230M07

QTY 3 OFF

M5

20

20

TO SHAPE FIT TO PART 12 PRIOR
TO DRILLING HOLE B SEE HEAD
ASSEMBLY DRAWING

REDUCE TO 8mm AFTER SHAPING

QTY 2 OFF

CLAMP PIECE 3

MATERIAL 16 DIAMETER
STEEL 230M07

8

16

TO SHAPE FIT TO PART 14 PRIOR
TO DRILLING HOLE B SEE HEAD
ASSEMBLY DRAWING

REDUCE TO 8mm AFTER SHAPING

QTY 1 OFF

TOMMY BAR 9

MATERIAL
5 DIAMETER STEEL 230M07

QTY 1 OFF

TOMMY BAR

100

COLUMNS 2

MATERIAL 10 DIAMETER STEEL 230M07

QTY 2 OFF

CLAMP PIECE 15

MATERIAL 16 DIAMETER
STEEL 230M07

8

16

MATERIAL 40 X 20 STEEL 070M20

DRILL HOLE B AFTER ASSEMBLY WITH PARTS
3, 15, 13 AND 14 NOTING DIMENSIONS ON
HEAD ASSEMBLY DRAWING.

HOLE SIZES
A. 5.2 2 OFF B. 12 1 OFF C. 16 2 OFF

QUANTITY 1 OFF

SPINDLE BEARING BLOCK 12
ASSEMBLE HEAD, PARTS 12, 13 AND 14, USING TWO PART RESIN ADHESIVE TO ENSURE HOLES ARE PARALLEL DO NOT REMOVE FROM THE VICE OR ANGLE PLATE BETWEEN DRILLING HOLES B

HEAD ASSEMBLY
MATERIAL 25 DIAMETER STEEL 230M07

HOLE A. 5.2 2 OFF  B. M4 2 OFF

12 AND 16 BORES MUST BE CONCENTRIC

QUANTITY 1 OFF

TAP CARRIER 10

HOLE A. 4.2 COUNTER BORE 7.5 DIAMETER 4.5 DEEP
B. 5.2 COUNTER BORE 9 DIAMETER 5.5 DEEP

MATERIAL 20 X 10 STEEL 070M20 QUANTITY 2 OFF

REAR BARS 17
MATERIAL 40 SQ STEEL 230M07

HOLES A. M5 2 OFF  
B. M5 4 OFF  
C. 10 2 OFF  

QUANTITY 1 OFF  
COLUMN BASE 18

MATERIAL 70 X 10 STEEL 070M20

QUANTITY 1 OFF  
HEAD CENTRE PIECE 13

HOLES A. M4  
B. 5.2 2 OFF DRILL IN PART 4 ONLY  
C. 5.2 2 OFF DRILL IN PART 5 ONLY

MATERIAL 20 X 10 STEEL 070M20

QUANTITY 1 OFF PART 4 1 OFF PART 5

CENTRE BARS 4 & 5

HOLES A. M4 3 OFF  

QUANTITY 4 OFF  

MATERIAL 20 X 10 STEEL 070M20

OUTER BARS 6